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ORIGINAL RESEARCH ARTICLE

Introducing Spin‑coated ZnO Anti‑refection Coating for CdS/CdTe Solar Cells

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Abstract

Second-generation solar cells, commonly known as thin-flm solar cells, have emerged as promising alternatives to traditional silicon-based frst-generation photovoltaic cells. The superstrate confguration is the most widely used structure for constructing thin-flm solar cells. Nevertheless, light refection from the front cover glass surface signifcantly contributes to energy losses in thin-flm solar cells. In this study, a ZnO anti-refection (AR) coating was introduced using the spin coating technique on a glass/FTO/CdS/CdTe/Cu/Au substrate to improve the power conversion efficiency of the solar cell by reducing front-surface refectance. The ZnO layer deposited at 3000 rpm in 15 s showed the minimum refectance and higher transmittance over a wavelength range of 500–900 nm. Further, the thickness of the film under optimal conditions was 63.32 nm, which is compatible with the ideal theoretical AR coating thickness of 65 nm. Comparing the device performance of the CdS/CdTe solar cell with and without AR coating, all tested devices showed an average short-circuit current density improvement of 6.8% and overall enhancement in power conversion efficiency of 9.3% .

Keywords AR coating · CdS/CdTe solar cell · refectance · spin coating

Introduction

Solar cell or photovoltaic cell technology is rapidly growing and poised to play an important role in global electricity generation in the near future. Even though solar cells have evolved through several generations, frst-generation solar cells, made of single- and multi-crystalline silicon, are the most common on the market due to their wide availability and high stability. However, higher manufacturing cost and lower power conversion efficiency (PCE) are key limitations of silicon-based solar cells.^{[1](#page-7-0)} Therefore, second-generation cadmium telluride solar cells (CdTe) have become the most

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prevalent thin flm type due to their lower cost and material requirements than traditional Si based solar cells. Additionally, the recorded laboratory-scale PCE of CdTe solar cells is 22.4%, which is competitive with the PCE of single-crystal silicon cells (27.6%) (27.6%) (27.6%) ^{2,[3](#page-7-2)} Therefore, integrating cost-effectiveness and ongoing research and development efforts to enhance efficiency will position CdTe solar cells as strong competitors to traditional silicon-based cells.

The PCE of these thin-flm solar cells is limited mainly due to the reflectance of light from their front surface. Thus, introducing ultrathin and transparent anti-refection (AR) flm coatings can ensure high PCE by reducing the refectance of light from the front surface of the solar cells. Previous studies have employed diferent kinds of materials such as ZnS , $SiO₂$, ZnO , MgO , and $TiO₂$ as AR coatings for photovoltaic cells using various deposition techniques. Gan-gopadhyay et al.^{[4](#page-7-3)} introduced a low-cost ZnS AR coating on monocrystalline silicon solar cells using the chemical bath deposition (CBD) technique, and reported that $I_{\rm sc}$ and PCE improved by 6.[5](#page-7-4)% and 5%, respectively. Similarly, Li et al.⁵ found that after introducing an electron beam-evaporated $SiO₂$ AR coating for silicon solar cells, the PCE was slightly improved from 17.48% to 17.8% . Sagar and Rao^{[6](#page-7-5)} reported

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that implementing radio-frequency (RF)-sputtered MgO and Al_2O_3 AR coatings on silicon solar cells increased their PCE from 8.33% to 9.86% and 8.38% to 9.13%, respectively. Pakhuruddin et al.⁷ investigated RF-sputtered ZnO AR coating on microcrystalline silicon solar cells, which provided minimum refectance at 600 nm of 2%, while liquid-phasedeposited (LPD) TiO₂ grown on silicon substrate exhibited an average minimum refectance of 2.7% at a wavelength range of 400–[8](#page-7-7)00 nm as reported by Wang et al.⁸

Research on single-layer AR coating for superstrate CdTe solar cells is notably rare in the literature. However, Kamin-ski et al.^{[9](#page-7-8)} undertook an experiment on quadruple-layer AR coating comprising $SiO₂$ and $ZrO₂$ for CdS/CdTe solar cells through DC magnetron sputtering. Their work yielded a 3% increase in current density, achieving a minimum refectance of 5% within the wavelength range of 500–600 nm. Employing the aforementioned AR coating materials and deposition technique, Law et al.¹⁰ fabricated a six-layer AR coating for CdSeTe/CdTe solar cells, yielding 3.45% enhancement in current density and 3.54% improvement in PCE. However, the total thickness of the AR coating of both studies was greater than 250 nm, which can lead to a reduction in the transmittance of the whole cell. In contrast to multilayer AR coatings, with careful selection of the appropriate AR coating material and thickness, a single-layer AR coating may provide a signifcant improvement in current density and PCE with minimal cost.

The thin-flm CdS/CdTe solar cells are developed using the superstrate configuration rather than the substrate configuration 11 to increase the light absorption, protection, and durability of the device. Therefore, the AR coating can be deposited on the top of the non-conductive side of the glass substrate before fabricating the solar cells or alternatively on the top of the complete device. However, the AR coating on the non-conductive side of the glass substrate prior to device fabrication can damage the AR coating during the solar cell material deposition process. Hence, it is advantageous to apply the AR coating after the solar cell has been fabricated.

In the present study, low-cost, nontoxic, wide-bandgap $(E_o \sim 3.37 \text{ eV})$ ZnO was tested as the AR coating for CdS/ CdTe solar cells due to its excellent transmittance in visible light, low resistance, optimum refractive index $(n \sim 2.0)$, and ability to grow using low-temperature deposition tech-niques.^{[12,](#page-8-1)13} To achieve cost-effective deposition of ultrathin and uniform ZnO AR coating on a non-conductive substrate at low temperatures, we chose the spin coating technique for the experiment.

Theoretical Evaluation

Single‑Layer AR Coating Design

Designing single-layer AR coating using theoretical calculations is advantageous prior to the fabrication. AR coatings are designed considering the relative phase shift between the incident beam refected at the upper and lower surfaces of the AR coating. Therefore, the optical thickness of the AR coating must be equal to a quarter of the incident light wavelength for zero reflectance, as indicated in Eq. $1.^{14}$ $1.^{14}$ $1.^{14}$ $1.^{14}$

$$
n_{AR}t = \frac{\lambda}{4} \tag{1}
$$

Since the refected beams have a180° phase shift, destructive interference cancels out both refected beams before they exit the surface (Fig. [1\)](#page-2-1).

The wavelength range considered in this experiment was 300–900 nm. However, a single-layer AR coating meets the minimum refectivity only at a single wavelength, not over the whole wavelength range. Consequently, the initial design focused on a narrow wavelength band where the higher radiation intensities of the solar spectrum occur. However, this approach is crucial for obtaining relatively low refectivity in a specifc wavelength range to achieve maximum power conversion efficiency of the solar cells.

Since the CdS window layer absorbs a higher portion of incident light at the 300–520 nm range before reaching the

Fig. 1 Destructive interference between refected beams.

Fig. 2 Absorbance spectrum of CdS and solar irradiance spectrum.

Fig. 3 CdS/CdTe solar cell structure with AR coating.

CdTe absorber layer, this study focused on the 500–900 nm wavelength range (Fig. [2](#page-3-0)) to minimize the front surface refectivity and enhance the PCE of solar cell. According to Fig. [2](#page-3-0), the maximum radiation intensity of the solar spectrum occurs between 450 nm and 550 nm wavelength. Therefore, obtaining minimum refectance at 520 nm is better for the initial design of the AR coating. In addition, according to Eq. [1,](#page-2-0) the thickness of the AR coating should be around 65 nm, assuming the refractive index of ZnO is about 2^{12} 2^{12} 2^{12}

Experimental Details

Deposition of the ZnO Layer

The thin-flm ZnO layer was deposited on the borosilicate glass substrate $(2.2 \times 2.5 \text{ cm}^2)$ as shown in Fig. [3,](#page-3-1) using spin coating.

Initially, the glass substrates were subjected to a cleaning process. Here, they were wiped with detergent, and then ultrasonically cleaned samples were immersed in acetone, methanol, and 2-propanol at a temperature of 80°C for

5 min, respectively, and fnally air-dried. Prior to the deposition of the ZnO thin flm, a saturated ZnO solution was prepared by dissolving 1.7 g of zinc acetate $(Zn(CH_3COO_2)$ in 25 ml of methanol followed by gravity-fltration. Before the spin coating process, borosilicate substrates were subjected to cleaning by O_2 plasma, which is a common technique for surface cleaning prior to bonding. Afterward, a set of thin-flm ZnO samples was spin coated at speeds of 1000–3500 rpm in steps of 500 rpm (the samples were denoted as S1, S2, S3, S4, S5, and S6) while keeping other parameters constant. The ZnO thin layer was developed by adding 0.75 ml of the $Zn(CH_3COO)$, dropwise into the center of the substrate immediately upon the start of spinning, which was maintained for 15 s. After the deposition, samples were heat-treated at 100°C for 120 min at atmospheric pressure in a tube furnace (GSL-1700X).

After the optimized deposition conditions were determined, the thin-flm ZnO coating was fabricated on a nonconducting glass substrate of the laboratory-developed glass/ fluorine-doped tin oxide (FTO)/CBD-CdS/CSS [close-spaced sublimation]-CdTe/Cu/Au solar cell.^{[15](#page-8-4)}

Characterization

The absorbance and transmittance spectra of the ZnO layers were obtained by UV–visible spectroscopy (PerkinElmer Lambda 365 UV/Vis spectrophotometer) in the wavelength range of 300–900 nm. The front surface refectance spectrum of the coated substrate was measured by a Bentham external quantum efficiency (EQE) setup (PVE300) to identify the best rpm value of the spin coater in order to achieve minimal refectance. Moreover, the thickness of the ZnO coating was measured by a proflometer (DektacXT). Then, atomic force microscopy (AFM) (Bruker Dimension Edge AFM) and energy-dispersive x-ray spectroscopy (EDAX Element) were performed to analyze the RMS roughness and identify the composition of the grown material of the optimized sample, respectively. Ultimately, the performance of the glass/FTO/CdS/CdTe/Cu/Au solar devices, with and without the AR coating, was measured under AM 1.5 illumination conditions (100 mW $cm⁻²$) using a solar simulator (PEC-L12).

Results and Discussion

Theoretical Background of the Formation of ZnO

The chemical reaction of zinc acetate $(Zn(CH_3COO)_{2} (s))$ and methanol $(CH₃OH$ (aq)) is an esterification reaction that produces byproducts of methyl acetate $(CH_3COOCH_3(aq))$ and zinc hydroxide $(Zn(OH)₂(aq))$, as represented in Eq. [2.](#page-4-0)

Fig. 4 Optical transmittance vs. wavelength plot of the ZnO AR coatings (S1 to S6).

Fig. 5 Tauc plot for the ZnO AR coatings S1 to S6.

$$
Zn(CH_3COO)_2(s) + 2 CH_3OH(aq) \rightarrow
$$

2 CH₃COOCH₃(aq) + Zn(OH)₂(aq) (2)

Since the boiling point of CH_3COOCH_3 (aq) is about $57^{\circ}C^{16}$ at standard atmospheric pressure (1 atm), at temperatures above 57°C, methyl acetate is vaporized. Here, when the spin-coated material is subjected to thermal annealing at 100 \degree C, ZnO (s) film is formed by dehydration of Zn(OH)₂ (aq) (Eq. [3](#page-4-1)).

 $Zn(OH)₂(aq) \rightarrow ZnO(s) + H₂O(g)$ (3)

Optical Properties

The optical transmittance values of the ZnO layers grown under the diferent spin rates are shown in Fig. [4](#page-4-2). Here, the ZnO layer deposited at low spin rates (S1 and S2) showed over 95% transmittance of light in the wavelength range of 500–900 nm. However, when the spin rate increased, the maximum transmittance (> 95%) occurred at a broader wavelength range. Consequently, the samples obtained at high spin rates (S5 and S6) showed over 95% transmittance of light in the wide optical range of 400–900 nm.

Figure [5](#page-4-3) presents the relevant Tauc plots for the growth of ZnO samples deposited at diferent spin rates. The ideal AR coating shows minimal absorbance across the spectrum, allowing most incident light to pass through the layer. The theoretical bandgap energy of ZnO is about 3.37 eV, 17 corresponding to a wavelength of 368 nm. Specifcally, ZnO is more transparent to light at wavelengths longer than 368 nm and absorbs light at shorter wavelengths (less than 368 nm). Table [I](#page-4-4) illustrates the energy bandgap values (E_{α}) of samples S1 to S6 determined from the Tauc plots. It is observed that the bandgap value increased slightly in proportion to the spin rate. Samples S1 and S2 have much lower bandgap values than their theoretical value (3.37 eV). However, the bandgaps of S4 to S6 reached closer to the theoretical value of ZnO.

Since this study aimed to obtain maximum transmittance within the wavelength range of 450–550 nm, where the solar spectrum exhibits higher intensity, the bandgap of ZnO was accurately aligned with the requirement. Samples S5 and S6, for which the ZnO layers were coated at 3000 rpm and 3500 rpm, respectively, and had higher light transmittance, were identifed as the best AR coatings in this study. After identifying samples S5 and S6 as possible AR coatings for the solar cell, all samples were subjected to refectance analysis to determine the selected AR coating deposition parameters.

The refectance spectrum of samples S1 to S6 in the wavelength range of 300–1000 nm is shown in Fig. [6](#page-5-0). The highest intensity peak of refectance was observed at a particular wavelength due to the phenomenon of constructive interference. The constructive interference occurs when waves refected from the front and back surfaces are in the same phase and result in an intense peak in the spectrum.

Table I The energy bandgap of samples S1 to S6 with respect to spin rate

As shown in Fig. [6,](#page-5-0) lower refectance was observed for samples S5 and S6 at a wavelength of 375 nm. Sample S5 exhibited the lowest refectance over the wavelength range of 500–900 nm. The lower the refectance, the better the light

Fig. 6 Refectance vs. wavelength plot of the ZnO AR coatings S1 to S6.

Fig. 7 Thickness of the ZnO AR coating vs. spin rate of deposition.

transmission; therefore, S5 was identifed as the optimal AR coating among the studied samples.

Variation in AR Coating Thickness

Figure [7](#page-5-1) shows the variation in the thickness of the ZnO layer with the spin rate. The thickness of the AR coating decreased (from around 90 nm to 55 nm) with the increase in the spin rate (1000–3500 rpm). When the thickness increased from 55 nm to 90 nm, the variation in light reflectance around 375 nm (Fig. 6) ranged from 21% (S1, 88.22 nm thickness) to 10% (S6, 57.62 nm thickness). Moreover, when the thickness of the AR coating increases, the optical path length that the light waves traverse through the coating also increases, which leads to maximizing the peak refectance.

The refectance of all samples tends to decline further after the peak point of the spectrum. This may occur due to destructive interference. As the thickness changes, minimum refectance due to destructive interference occurs at diferent wavelengths of the samples S1 to S6 in the 300–900 nm wavelength region as shown in Table [II](#page-5-2).

According to Table II , the minimum reflection was shifted towards a shorter wavelength when thickness was reduced. The minimum refectance of 2.5% at 570 nm was observed from sample S5, which has a thickness of 63.32 nm. Hence, sample S5 fulflled the requirement for AR coating having a value closer to the calculated theoretical value (65 nm) in the initial experimental design. This further validated the results of the initial design.

However, according to Fig. [6](#page-5-0) and Table [II](#page-5-2), sample S6 shows greater refectance than sample S5 despite having lower thickness than S5. As the thickness decreases beyond its optimum value, the coating may become less able to interfere destructively with incoming light waves, resulting in increased refectance. Therefore, further reduction of the thickness beyond 63.32 nm may not be efective in reducing the refectance.

Surface Analysis

After identifying the best AR coating for sample S5, further analysis was performed to determine the surface topography and elemental analysis. Figure [8](#page-6-0) shows the AFM images of ZnO spin-coated at 3000 rpm (S5). The root-mean-square

Table II Minimum refectance with corresponding wavelength of the samples S1 to S6

Fig. 8 (a) 3D and (b) 2D AFM images of ZnO surface deposited at 3000 rpm.

Table III Composition of ZnO sample grown on FTO/glass substrate

Element	Weight $(\%)$	Atomic $(\%)$	
Ω	13.75	48.55	
Si	5.09	10.23	
Sn	74.47	35.44	
Zn	6.68	5.77	

(RMS) roughness of sample S5 was measured as 11.44 nm, while the roughness of the bare surface was 7.86 nm. Hence, it is evident that the resultant increase in substrate roughness is due to the ZnO AR coating. This AR coating may enhance the light-trapping ability of the device. When light hits the device, some light can be refected due to the refractive index diference between the two mediums. The presence of a rough surface can cause multiple refections and increase light entering the device, leading to improved current density and power conversion efficiency.

Elemental Analysis

The composition of the glass/FTO/ZnO substrate is shown in Table [III](#page-6-1). The ZnO layer was deposited on the FTO layer for convenience of measurement. Accordingly, the formation of ZnO was confrmed.

Device Characterization

The laboratory-developed glass/FTO/CBD-CdS/CSS-CdTe/ Cu/Au device^{[15](#page-8-4)} was then completed by depositing the AR coating of ZnO following the preparation of sample S5. Three replicates were used for the device performance

Fig. 9 *J*–*V* curves for device 1 with and without AR coating.

measurements. Figure [9](#page-6-2) shows the current density vs. voltage (*J*-*V*) curve of one device with and without AR coating. After introducing the AR coating, the light passing through the coating and into the cell increased due to a reduction in refectance, which allows more photons to absorb into the device, leading to a higher generation of electron-hole pairs. As a result, more charge carriers are available, thereby increasing the current density. Therefore, after deposition of the AR coating, the current density increased from 37.1 mA cm−2 to 39.8 mA cm−2, resulting in an increase in PCE from 11.9% to 13.2%.

The experimental findings for additional devices are detailed in Table [IV,](#page-7-10) indicating average improvements in

		$J_{\rm SC}$ (mA cm ⁻²)	$J_{\rm SC}$ improvement (%)	PCE $(\%)$	PCE improvement $(\%)$
Device 1	Bare	37.1	7.3	11.9	10.9
	With AR	39.8		13.2	
Device 2	Bare	35.5	6.2	13.4	9.0
	With AR	37.7		14.6	
Device 3	Bare	37.2	6.2	13.9	7.9
	With AR	39.8		15.0	
Device 4	Bare	34.8	7.7	12.2	9.8
	With AR	37.6		13.4	
Device 5	Bare	37.2	6.7	13.3	8.2
	With AR	39.7		14.4	
Device 6	Bare	37.7	6.9	12.3	9.8
	With AR	40.3		13.5	
	Average		6.8		9.3

Table IV Comparison of device performance with and without AR coating

current density and PCE of 6.8% and 9.3%, respectively. The results show that the enhancement in device performance after ZnO single-layer AR coating deposition has surpassed the recorded values in multilayer AR coatings introduced for CdTe-based solar cells.

Conclusion

In this study, optimal conditions for the growth of ZnO AR coating using the spin coating technique were identifed as 3000 rpm for 15 s using a zinc acetate precursor dissolved in methanol. Furthermore, minimal refectance (2.5%) and surface roughness (11.44 nm) confrmed the suitability of the growth of ZnO as an AR coating. Additionally, after introducing the optimized ZnO AR coating, the average current density and power conversion efficiency of the laboratorydeveloped CdS/CdTe solar cells were enhanced by 6.8% and 9.3%, respectively. Therefore, spin-coated ZnO is an ideal AR coating for CdS/CdTe solar cell devices.

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Author contributions All authors contributed to the study conception and design. Material preparation, data collection and analysis were performed by J.R. Wijesingha, G.K.U.P. Gajanayake and W.A.V.U. Wickramasinghe. R.M.T Damayanthi, G.I.P De Silva, and D.S.M. De Silva revised the manuscript. The frst draft of the manuscript was written by J.R. Wijesingha, and all authors commented on previous versions of the manuscript. All authors read and approved the fnal manuscript.

Data availability The datasets analyzed during the current study are available from the corresponding author upon reasonable request.

Conflict of interest On behalf of all authors, the corresponding author states that there is no confict of interest.

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